

Self-standing process by using bimetallic effect of thin-film metallic glass

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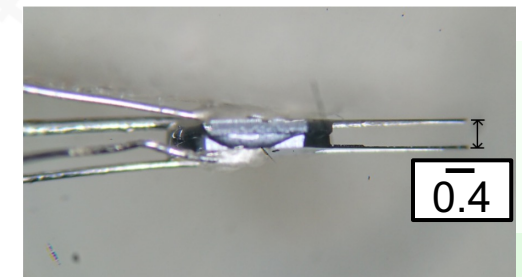
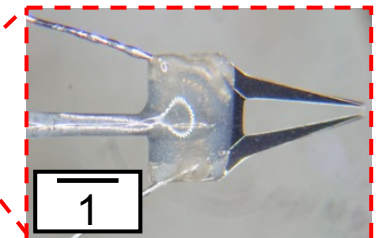
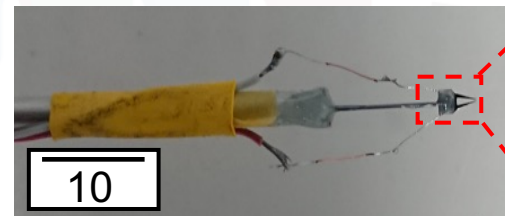
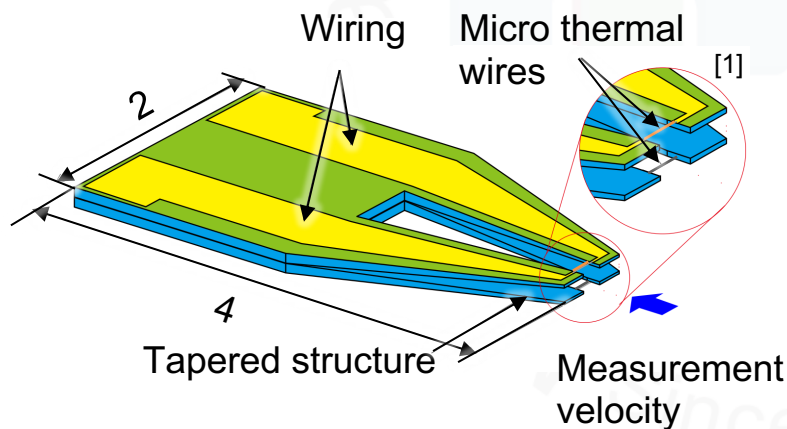
1. Introduction

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Background

The microprobe hot-wire velocimeter [1]

- Aiming to **improve fuel efficiency** of engines and turbines
- Micro thermal wires placed at the tip (sensing area)
- Heated thermal wires cooled by air flow
 - **Measuring flow velocity and gas concentration from output of voltage change of hot wires**



Background

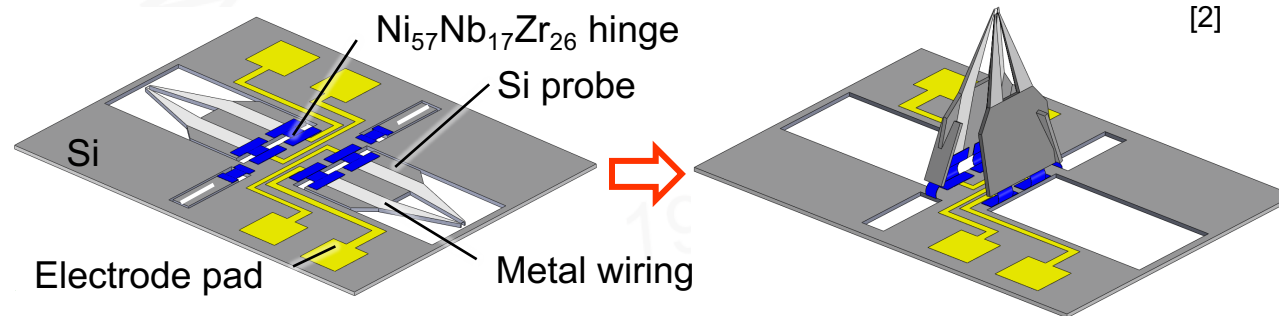
Problems in the previous study

- Manual assembly of probes fabricated by planar process
- Difficult to achieve 3D structures with conventional processes
 - Integration for multi-component flow velocity measurement
 - Need to face the hot wire vertically in flow velocity measurement

Fabrication of 3D structures by self-assembly process

Development of a new fabrication process for 3D micro forming

- The probe is self-supporting at a deformation angles of over 90° relative to the substrate.



[2] Nagai R, Onishi T, Oka C, Sakurai J and Hata S 2022 Self-standing process for microprobes
Proceedings of JSME International Conference of Materials and Processing 2022



3D micro forming using thin-film metallic glass (TFMG)

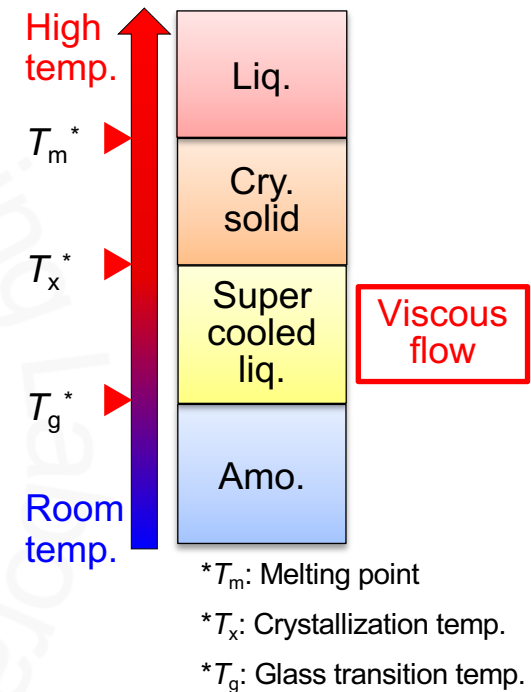
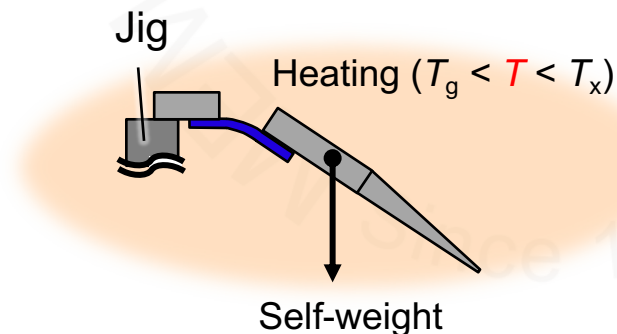
Metallic glass

- Deformed by **viscous flow** in supercooled liquid range
 $T_g < T < T_x$
- Conductive, **enabling 3D wiring**

Molding by heating-deformation method

Molding process by using viscous flow during heating, applying an external force

- Utilizing **the self-weight** of the Si probe
- **Difficult to achieve greater than 90°**

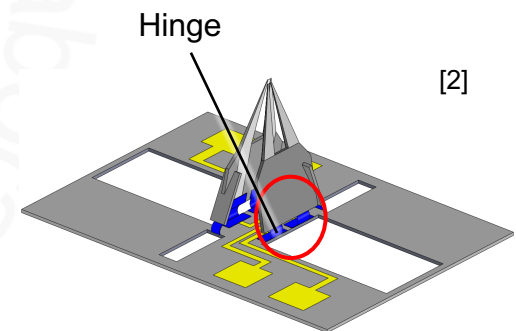


Purpose

Investigation of self-assembly process of 3D MEMS structure for ultra-small flow velocity sensors

Contents

- Fabrication of samples for investigation of self-standing microstructures
 - Fabrication process
 - Results of fabrication
- Improving angles of deformation
 - Improvement by using bimetallic effect of metallic glass
 - Results of deformation
 - Causes of deformation irregularity



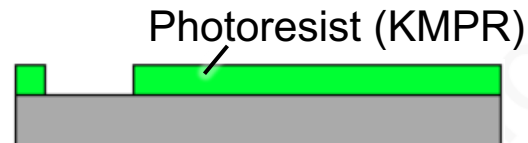
[2] Nagai R, Onishi T, Oka C, Sakurai J and Hata S 2022 Self-standing process for microprobes
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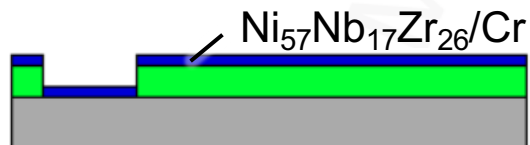
2. Sample fabrication

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Fabrication process



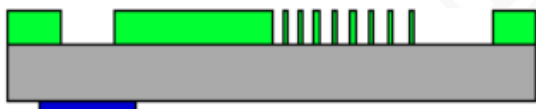
1. Patterning photoresist



2. Sputtering TFMG



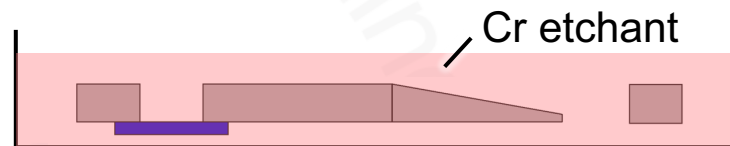
3. Lift-off TFMG



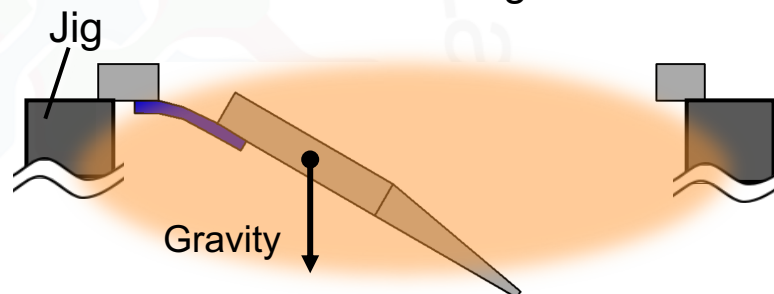
4. Patterning photoresist



5. DRIE



6. Cr etching



7. Heating (560°C - 5 min) $T_g : 557^\circ\text{C}$



8. Cooling

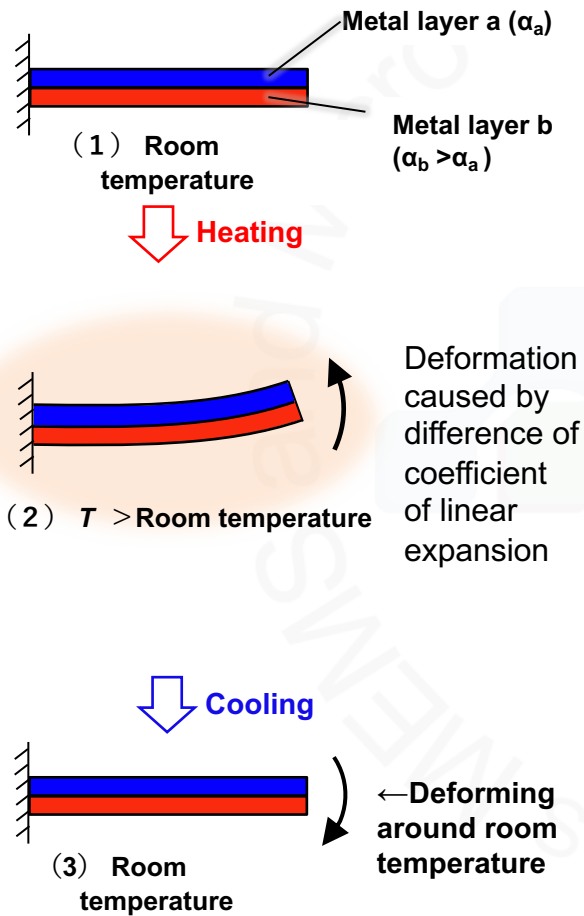


3. Improving angles of deformation

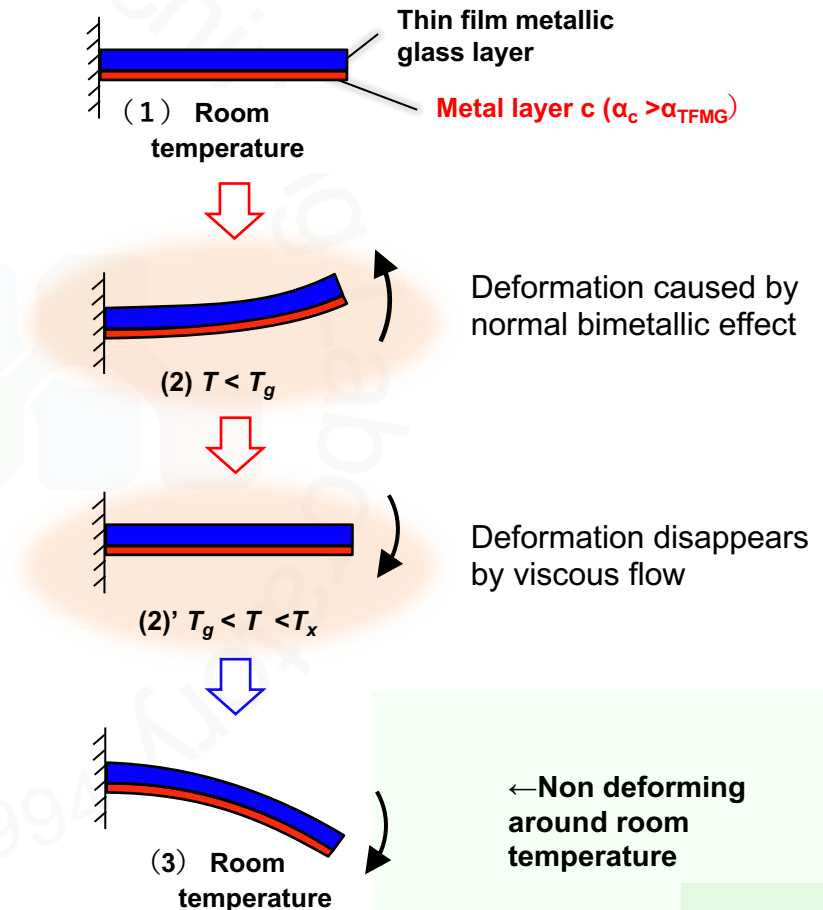
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Bimetallic effect of Thin-film metallic glass

- Elastic materials



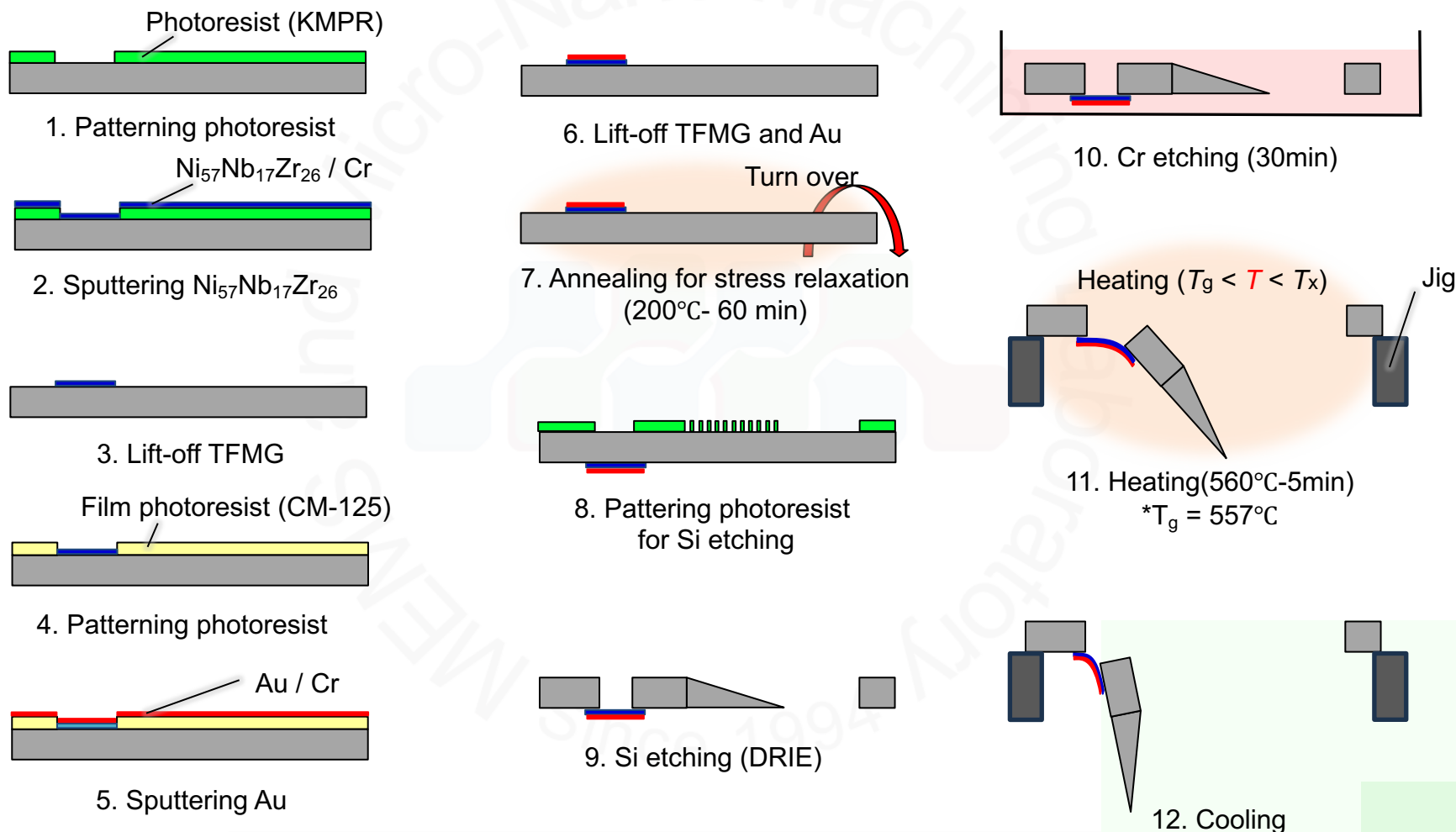
- Thin-film metallic glass



3. Improving angles of deformation

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Fabrication process for utilizing bimetallic effect



3. Improving angles of deformation

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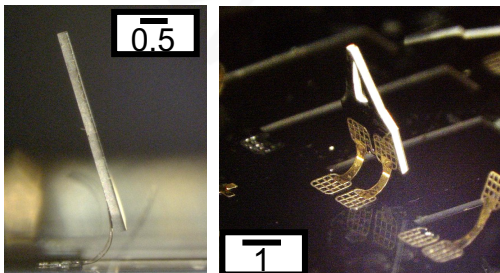
Results of deformation

Heating treatment conditions

- Temperature : 560°C ($*T_g = 557^\circ\text{C}$)
- Heating rate : 20 K / min
- Heating time : 5 min

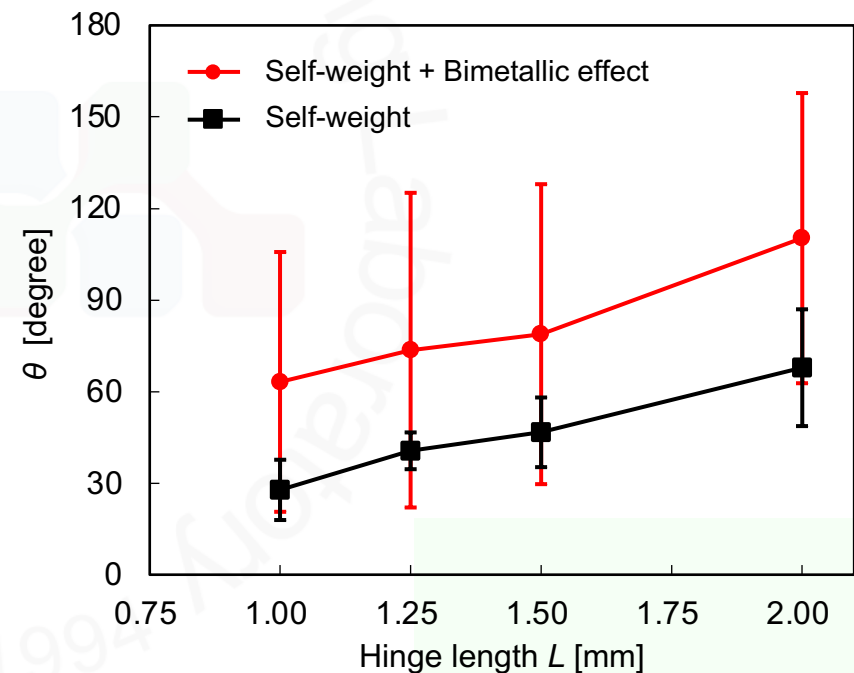
Results

- **Increasing** deformation angles
- **Max deformation 157.3° ($L = 2.00$ mm)**
- **Significant deformation irregularity**
 $77.6^\circ \pm 44.8^\circ$ ($L = 1.00$ mm)



$L=1.00, 107.5^\circ$

[2] Nagai R, Onishi T, Oka C, Sakurai J and Hata S 2022 Self-standing process for microprobes
Proceedings of JSME International Conference of Materials and Processing 2022



3. Improving angles of deformation

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Causes of deformation irregularity

Expected factors

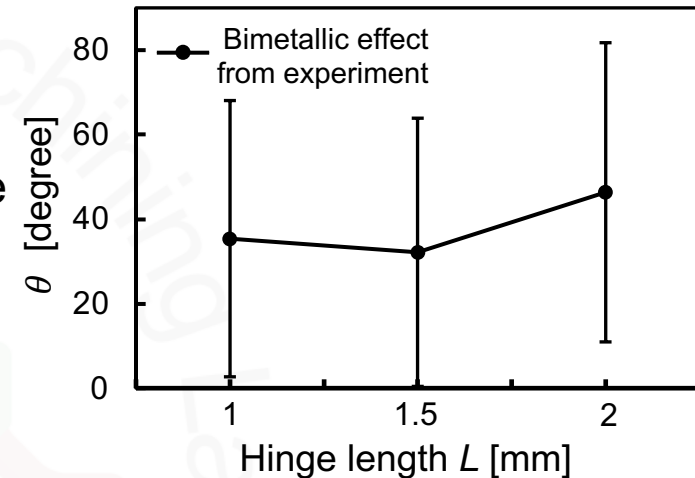
- **Film thickness** variation in both layers
- Variation of **heating temperature** on a substrate

Investigation of film thickness

- To assess thickness variations of each layer

Simplified model analysis

- To consider the effect of film thickness and heating temperature on deformation
- Uncovering tendency of deformation on each parameters



3. Improving angles of deformation

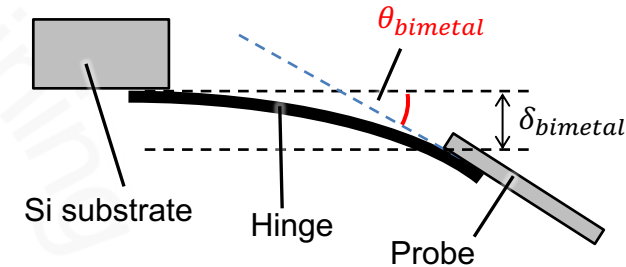
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Causes of deformation irregularity

Analysis of the bimetallic effect

$$\theta_{bimetal} = \frac{6E_1(T - T_0)(\alpha_1 - \alpha_2)th_1}{2th_1E_1(2h - h_1) + \eta h(h - h_1)} l^{[3]} \quad (1)$$

$$\ln \eta = \ln 7.0 + \left(30 - \frac{T}{20}\right) \ln 10 \quad (2)$$



$\theta_{bimetal}$: Deflection angle l : Hinge length, t : Deformation time, η : Viscosity of TFMG layer
 E_1, E_2 : Young's modules of Au and TFMG layer
 α_1, α_2 : Coefficients of Liner Thermal Expansion of Au and TFMG layer
 T, T_0 : Heating temperature, Original temperature h_1, h_2, h : Thickness of Au, TFMG layer and bimetallic layer

Variables

- Hinge length $L = 1.0, 1.5, 2.0$ mm, Heating temperature $T = 560 \text{ }^\circ\text{C} \pm 2\%$ ($548.8^\circ\text{C} - 571.2^\circ\text{C}$)
- Thickness of Au layer $h_1 = 1 \text{ } \mu\text{m} \pm 10\%$
- Thickness of TFMG layer $h_2 = 10 \text{ } \mu\text{m} \pm 10\%$

	Young Modules [GPa]	Coefficient of liner expansion [1/K]	Viscosity [GPa·s]	Length of hinge [mm]	Temperature [C°]	Time [s]
Au Layer	78	14.2×10^{-6}	—	L	T	300
Ni-Nb-Zr Layer	30	8.00×10^{-6}	η			

[3] Hata S, Goto J, Sato K, Shimokobe A 2000 Fabrication of Micro Structures using Thin Film Metallic Glass
 - Fabrication of Thin Film Metallic Glass and Micro-Forming using the Supercooled Liquid State -



3. Improving angles of deformation

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Causes of deformation irregularity

Analysis of the bimetallic effect

- Conditions for maximum deformation angles

$$\theta_{bimetal} = 62.1 \text{ deg}$$

$$L = 2.0 \text{ mm}, T = 571.2^\circ\text{C},$$

$$h_1 = 0.9 \text{ }\mu\text{m}, h_2 = 9 \text{ }\mu\text{m}$$

h_1 : Thickness of Au Layer, h_2 : Thickness of TFMG Layer

- Deformation irregularity : proportional to hinge length

⇒ The smallest hinge length with a deformation angle of greater than 90°

- Greatest factor for deformation : **Temperature**
- Second greatest factor for deformation : **Thickness of TFMG Layer**

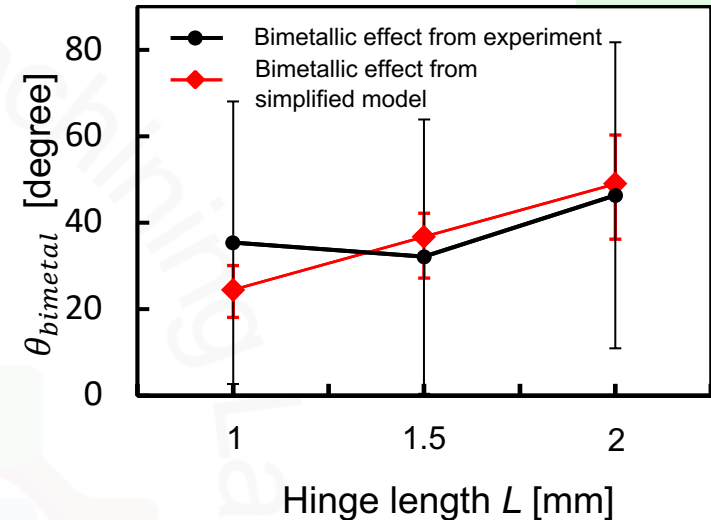


Table 1. Condition for the upper one-third deformation angle at hinge length $L = 2.0 \text{ mm}$

Deflection angle [deg]	Au layer thickness [μm]	TFMG layer thickness [μm]	Temperature [°C]
62.1	0.9	9	571.2
61.9	1	9	571.2
61.6	1.1	9	571.2
56.1	0.9	10	571.2
55.9	1	10	571.2
55.7	1.1	10	571.2
52.9	1.1	9	560
52.6	1	9	560
52.2	0.9	9	560



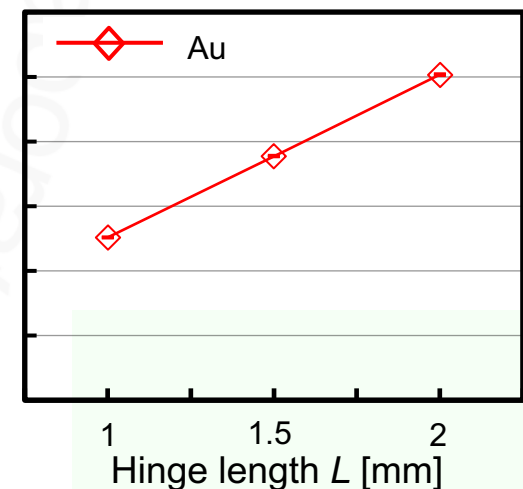
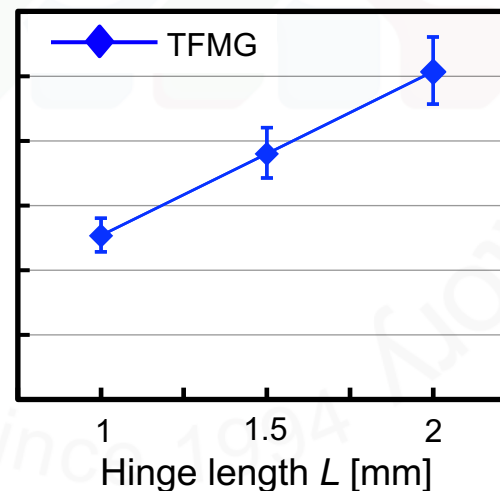
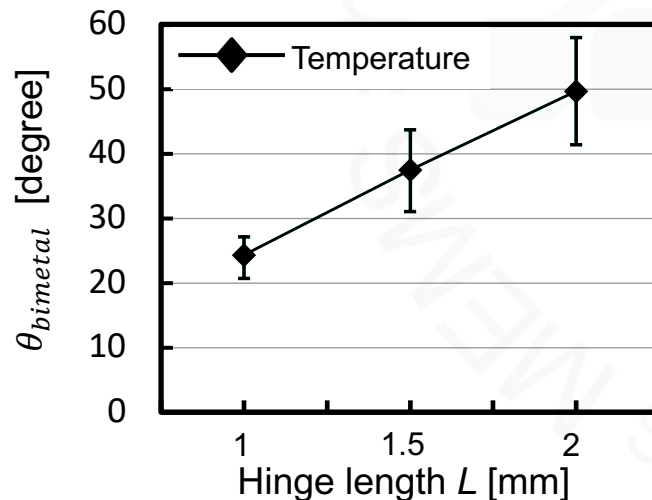
3. Improving angles of deformation

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Causes of deformation irregularity

Comparison of respective parameters

- $T = 560^{\circ}\text{C} \pm 2\%$ ($548.8^{\circ}\text{C} \sim 571.2^{\circ}\text{C}$), $h_2 = 10\text{ }\mu\text{m} \pm 10\%$, $h_1 = 1\text{ }\mu\text{m} \pm 10\%$
* h_2 : Thickness of TFMG Layer, h_1 : Thickness of Au Layer
 - Largest contributor : Temperature
 - Low effect by Thickness of Au layer
- ⇒ Attention should be paid to the heating temperature.



Conclusions

We investigated the basic process for fabricating self-standing microstructures using $\text{Ni}_{57}\text{Nb}_{17}\text{Zr}_{26}$ thin-film metallic glass (TFMG).

- Deformation was **not enough** with simple TFMG hinge.
- Deformation **greater than 90°** was achieved by depositing Au layer on TFMG layer as a bimetallic layer.
- **Significant deformation irregularity** has happened.
- Attention should be paid to heating temperature.

Future works

- Conducting experiments to investigate the effect of heating temperature on the deformation angle.
- Improving deformation accuracy by control the thickness of both layers and heating temperature
- Realizing self-standing 3D structure
- Self-assembly using the surface tension of molten solder

