

# Free Spectral Range Measurement of Fabry-Perot Cavity Using Transmission Light, Single Frequency Modulation and Null Method Under Off-resonance Condition

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## Abstract

In this paper, we propose a novel method to measure the free spectral range (FSR) of a Fabry-Perot cavity (FPC) using frequency modulation (FM) with an electric optical modulator (EOM) and the null method. A laser beam modulated by the EOM, to which a sine-wave signal is supplied from a radio frequency (RF) oscillator, is incident on the FPC. The transmission light from the FPC is observed and converted to an RF signal by a high-speed photodetector, and the RF signal is synchronously demodulated with a lock-in amplifier (LIA) by referring to the oscillator. We theoretically and experimentally demonstrate that the LIA signal become null with a steep slope, when the modulation frequency equals the FSR under the condition that the carrier frequency of the laser is slightly detuned from the resonance of the FPC.

## 1 Introduction

In the future, an absolute length measurement method with a measurement range of 1 meter or more and an accuracy of sub-nanometer order or less will be required, due to the progress of nanotechnology and ultraprecision engineering. To overcome this problem, many researchers have developed absolute length measurement methods with a small measurement uncertainty<sup>[1],[2],[3]</sup>. Since the free spectral range (FSR) of a Fabry-Perot cavity (FPC) is inversely proportional to the optical distance between the two mirrors of the FPC, the FSR measurement method may be an alternative candidate for absolute length measurements<sup>[2],[3]</sup>. In this paper, a novel FSR measurement method using the interference between a carrier and frequency modulation (FM) sidebands is proposed. In our method, the FSR can be determined from the null method using transmission light and the FM technique under the condition that the carrier frequency is slightly detuned from the resonance of the FPC.

## 2 Measurement principle

A conventional FPC consists of two mirrors separated by a distance of  $L$ . Its FSR ( $f_{FSR} = \omega_{FSR}/2\pi$ ) is defined as

$$f_{FSR} = \frac{\omega_{FSR}}{2\pi} = \frac{c}{2n_c L} \quad (1),$$

where  $c$  and  $n_c$  are the velocity of light in a vacuum and the refractive index of the medium inside the cavity. If the  $f_{FSR}$  or  $\omega_{FSR}$  is measured, then the absolute optical length ( $n_c L$ ) can be determined using Eq. (1). Fig. 1 shows the basic FSR-measuring system discussed in this paper. In the figure, ECLD, EOM, PD, OSC and LPF are an extra cavity laser diode, an electric optical modulator, a photodetector, an oscillator and a low-pass filter, respectively. A lock-in amplifier (LIA) consists of a mixer and the LPF.

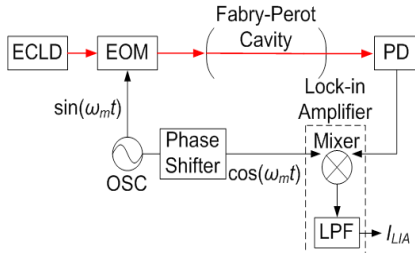


Fig. 1 Basic FSR measuring system.

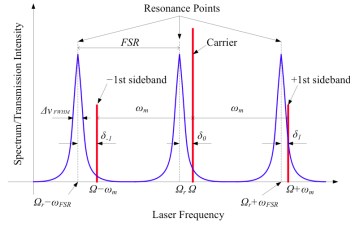


Fig. 2 Relationship between FPC transmission, carrier (0-th) and FM sidebands ( $\pm 1$ th).

The electric field  $E_{EOM}(t)$  modulated by the EOM is represented as

$$E_{EOM}(t) = E \left[ \sum_{n=-\infty}^{\infty} J_n(m) \exp[i(\Omega + n\omega_m)t] \right] \quad (2),$$

where  $E$ ,  $\Omega$ ,  $m$  and  $J_n$  are the original electric field of the ECLD, its carrier frequency, the modulation depth and the  $n$ -th order Bessel function, respectively. Fig. 2 shows the relationship between FPC transmission, carrier and two FM sidebands. In Fig. 2,  $\Omega_r$  and  $\Delta\nu_{FWHM}$  are the main resonance frequency closest to the carrier frequency  $\Omega$  and the full width at half maximum of the resonance curve, respectively. As shown in Fig. 2, the detuning frequency shifts  $\delta_n$  ( $n = 0, \pm 1, \pm 2, \dots$ ) between resonance frequencies and the FM sidebands can be written:

$$\begin{aligned}\delta_n &= (\Omega + n\omega_m) - (\Omega_r + n\omega_{FSR}) \\ &= \delta_0 + n(\omega_m - \omega_{FSR})\end{aligned}$$

(3),

where  $\delta_0$  is  $(\Omega - \Omega_r)$ . Eq. (3) can be rewritten by normalizing it relative to the  $\omega_{FSR}$  as follows:

$$\bar{\delta}_n = \bar{\delta}_0 + n(\bar{\omega}_m - 1)$$

(4),

$$\text{where } \bar{\delta}_n = \frac{\delta_n}{\omega_{FSR}}, \bar{\delta}_0 = \frac{\delta_0}{\omega_{FSR}}, \bar{\omega}_m = \frac{\omega_m}{\omega_{FSR}}.$$

When an arbitrary optical field  $E_i$  is incident on a lossless FPC, the transmission field  $E_t$  is approximately given by<sup>[3],[4]</sup>

$$E_t = \frac{E_i}{1 + 2iF\bar{\delta}} = T_{FPC}(\bar{\delta})E_i \quad (T_{FPC}(\bar{\delta}) = \frac{1}{1 + 2iF\bar{\delta}}) \quad (5),$$

where  $\bar{\delta}$ ,  $F$  and  $T_{FPC}$  are the normalized detuning frequency from the cavity resonance, the cavity finesse and the amplitude transmission function of the FPC, respectively. If the electric field  $E_{EOM}(t)$  given by Eq. (2) is incident on the FPC, then, using Eq. (5), the transmitted electric field  $E_{FPC}(t)$  is given by

$$E_{FPC}(t) = E \sum_{n=-\infty}^{\infty} [J_n(m) T_{FPC}(\bar{\delta}_n) \exp\{i(\Omega + n\omega_m)t\}] \quad (6),$$

where a dispersion effect of the FPC is neglected. Therefore, the transmitted intensity  $I_{FPC}(t)$  is written as

$$\begin{aligned}I_{FPC}(t) &= |E|^2 \sum_{n=-\infty}^{\infty} [J_n(m)]^2 |T_{FPC}(\bar{\delta}_n)|^2 \\ &+ 2|E|^2 \sum_{n=0}^{\infty} [J_n(m)J_{n+1}(m)] \{ \text{Re}[T_{FPC}(\bar{\delta}_n)T_{FPC}^*(\bar{\delta}_{n+1}) - T_{FPC}^*(\bar{\delta}_n)T_{FPC}(\bar{\delta}_{n-1})] \cos\omega_m t \\ &\quad + \text{Im}[T_{FPC}(\bar{\delta}_n)T_{FPC}^*(\bar{\delta}_{n+1}) - T_{FPC}^*(\bar{\delta}_n)T_{FPC}(\bar{\delta}_{n-1})] \sin\omega_m t \} \\ &+ (\text{higher than } 2\omega_m \text{ terms})\end{aligned} \quad (7),$$

The LIA signal  $I_{LLAc}$  for  $\cos\omega_m t$  term is represented as,

$$I_{LLAc} = k_{LLA} |E|^2 \sum_{n=0}^{\infty} [J_n(m)J_{n+1}(m)] \left\{ \frac{1 + 4F^2\bar{\delta}_n\bar{\delta}_{n+1}}{(1 + 4F^2\bar{\delta}_n^2)(1 + 4F^2\bar{\delta}_{n+1}^2)} - \frac{1 + 4F^2\bar{\delta}_n\bar{\delta}_{n-1}}{(1 + 4F^2\bar{\delta}_n^2)(1 + 4F^2\bar{\delta}_{n-1}^2)} \right\} \quad (8),$$

where  $k_{LLA}$  is the amplification constant of the LIA. The LIA signal  $I_{LLAc}$  must cross the null when the modulation frequency equals the FSR of the FPC and the carrier frequency is slightly detuned from the resonance. The optimum carrier detuning shift ( $\delta_0$ ) for the steepest slope is approximately 29% of  $\Delta\nu_{FWHM}$ .

### 3 Experimental results

In the experiment, we used the ECLD (NewFocus 6304, center wavelength = 633 nm, power = 1 mW), the EOM (JEOPTIK Laser PM633), the OSC (Anritsu 3641A), the FPC (Neoark 2221), an avalanche PD (Hamamatsu Photonics C5658), LIA (=a passive double-balanced mixer (R&K MX130-0S) + an LPF (NF Corporation E-3201, cut-off frequency = 1 kHz)). The modulation frequency of the OSC was measured by a frequency counter (Pendulum CNT-90, not shown in Fig. 1). The LIA signal and the modulation frequency were simultaneously recorded with a personal computer. The FSR and finesse of the FPC in a normal temperature of 293 K in the specification are approximately 888.9 MHz and 142, respectively. In the experiment, the modulation depth  $m$  was adjusted to approximately 1.08 rad.

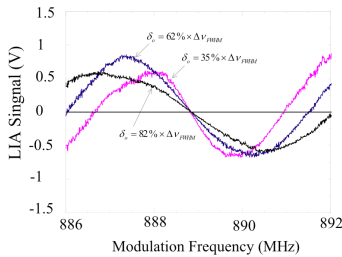


Fig. 3 Relationships between modulation frequency and LIA signal. Frequency scan step = 20 kHz/step.

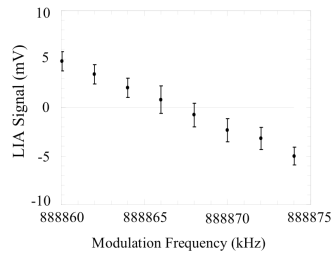


Fig. 4 Relationship between modulation frequency and LIA signal. Frequency scan step = 2 kHz/step.

Fig. 3 shows the measured relationships between the modulation frequency and the LIA signal  $I_{LIAc}$ . In Fig. 3, the results for the three detuning frequency shifts ( $\delta_0$ ), 35, 62 and 82% of  $\Delta V_{FWHM}$ , are shown. Fig. 4 shows the detailed relationship between the modulation frequency and the LIA signal  $I_{LIAc}$  for the case of a detuning shift ( $\delta_0$ ) of 35% of  $\Delta V_{FWHM}$ . From Fig. 4, the FSR was determined to be 888867 kHz ( $n_c L = 168.637$  mm). The estimated uncertainty was  $10^{-6}$  order.

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